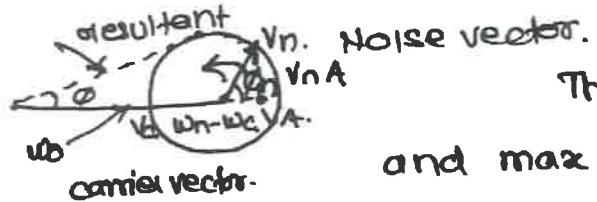


subject: Principles of Analog and Digital Commn

Q1. solve any four [5M each] [20M]

Ans a. Compare Analog and digital communication  
[5 points 5 marks each]

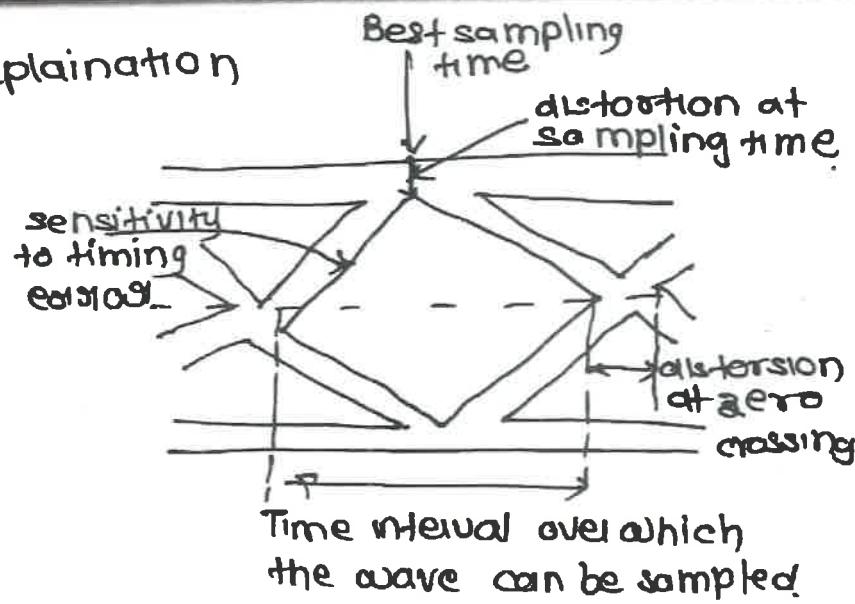
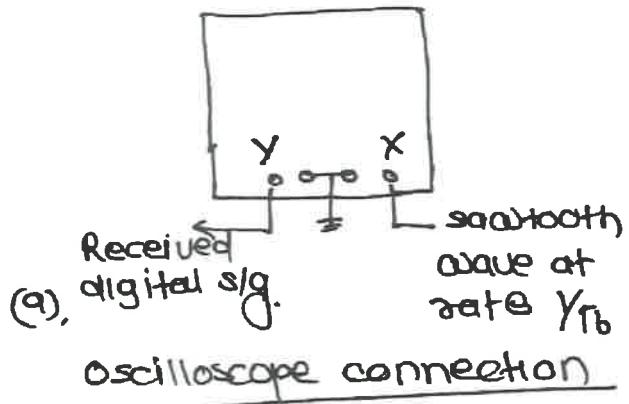
Ans b. Noise triangle explanation. [5M]



The max. deviation in amp =  $V_n$ .

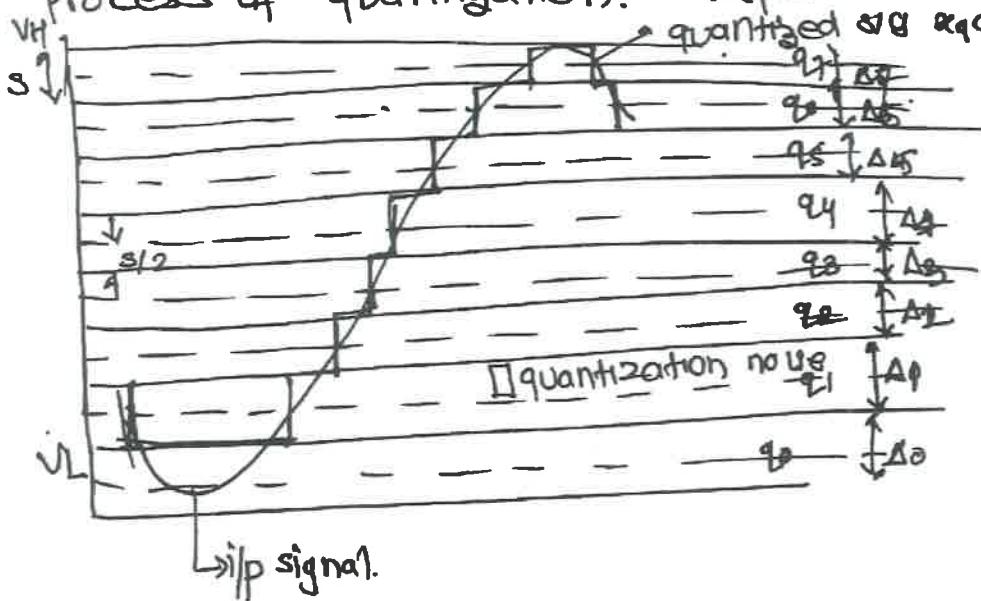
and max. deviatn in  $\phi = \phi = \sin^{-1}(V_n/V_c)$

Ans c. Eye pattern. Explanation



(b) Interpretation of eye pattern.

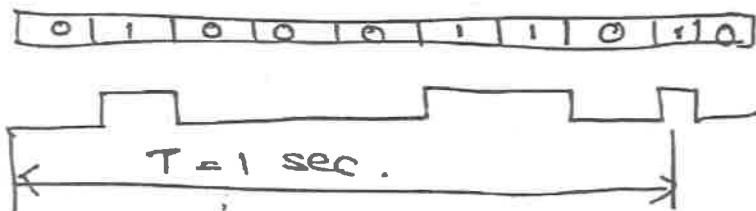
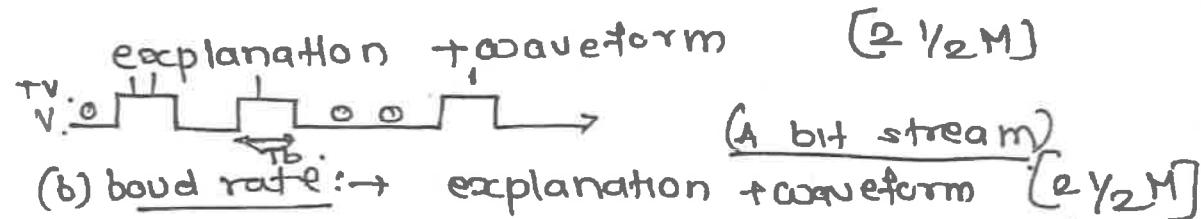
Ans d. process of quantization. explanation [3 + 2 diag] = 5M





Q2

Ans e: (a) bit rate:  $\frac{1}{T_b}$   
bit interval).



Q2. (a)	shot noise	explanation	$[2 \frac{1}{2} M]$
	Equivalent noise temp	"	$[2 \frac{1}{2} M]$
	<u>Derivation</u>	"	$[2 \frac{1}{2} M]$

The noise at the i/p of amp is given by.

$$P_{na} = (F-1) k T_0 B.$$

This is noise contributed by the amp.

This noise can be alternately represented by some fictitious temp  $T_{eq}$ .

$$P_{na} = k T_{eq} B.$$

$$k T_{eq} B = (F-1) k T_0 B$$

$$\therefore T_{eq} = (F-1) T_0$$

Numerical:

$$F = 10 \log_{10} f = \text{Antilog of } (0.5) \quad [2 \frac{1}{2} M]$$

$$f = 10^{0.5} \times 2.$$

$$T_{eq} = (F-1) T_0 = (2-1) \times 300 = 300^{\circ} K.$$

$$\boxed{T_{eq} = 300^{\circ} K.}$$



Ques 2

(2)

Ans b :-

(1) Time shifting :-

[5M]

The time shifting property states that if  $x(t)$  and  $x(t)$  form a FT pair then

$$x(t-t_0) \leftrightarrow e^{-j2\pi f t_0} X(f).$$

∴ Here the signal  $x(t-t_0)$  is a time shifted sig.  
It is the same sig  $x(t)$  only shifted in time.

Proof:  $F(x(t-t_0)) = \int_{-\infty}^{\infty} x(t-t_0) e^{-j2\pi f t} dt.$

$$\text{Let } (t-t_0) = \underbrace{\downarrow}_{\text{---}} T$$

$$\therefore f = \frac{1}{T}$$

$$dt = dT$$

$$\therefore F[x(t-t_0)] = \int_{-\infty}^{\infty} x(T) e^{-j2\pi f(t+T)} dT$$

$$= e^{-j2\pi f t_0} \int_{-\infty}^{\infty} x(T) e^{-j2\pi f T} dT.$$

$$F[x(t-t_0)] = e^{-j2\pi f t_0} X(f)$$

This shows that time shifting does not have any effect on the ampl. spectrum, but there is an additional phase shift of  $-2\pi f t_0$ . which is denoted by term  $e^{-j2\pi f t_0}$ .

(2) Differentiation in time domain [5M]

This property is applicable if and only if the derivative of  $x(t)$  is Fourier transformable

Statement:- Let  $x(t) \leftrightarrow X(f)$ . and let derivative of  $x(t)$  be Fourier transformable.

$$\frac{d}{dt} x(t) \leftrightarrow j2\pi f X(f).$$

$$x(t) = \int_{-\infty}^{\infty} X(f) e^{j2\pi f t} df$$

$$\therefore \frac{d}{dt} x(t) = \frac{d}{dt} \left[ \int_{-\infty}^{\infty} X(f) e^{j2\pi f t} df \right] = \int_{-\infty}^{\infty} X(f) \left( \frac{d}{dt} e^{j2\pi f t} \right) df$$

$$\frac{d}{dt} x(t) = \int_{-\infty}^{\infty} [X(f) \cdot j2\pi f] e^{j2\pi f t} df.$$

As per the def'n of the inverse F.T the term inside the sq. bracket must be the FT of  $\frac{d}{dt} x(t)$

$$\therefore F \left[ \frac{d}{dt} x(t) \right] = j2\pi f X(f)$$

$$\text{OR } \frac{d}{dt} x(t) \xrightarrow{F} j2\pi f X(f).$$

Q3.(a)  $P_c = 400 \text{ W}$ ,  $R_L = 50 \Omega$   $m = 0.8$ ,  $f_m = 5 \text{ kHz}$ ,

$$f_c = 1 \text{ MHz}$$

(1) carrier amplitude  $V_c$ .

$$\therefore \text{The carrier power } P_c = \frac{V_c^2}{2R_L}$$

$$V_c = \sqrt{2R_L P_c} = \sqrt{2 \times 50 \times 400} = 200 \text{ Volts.}$$

(2) Expression for AM wave

$$e_{AM} = E_c [1 + m \cos(2\pi f_m t)] \cos(2\pi f_c t)$$

$$E_c = 200 \text{ V} \quad m = 0.8 \quad f_m = 5 \text{ kHz} \quad f_c = 1 \text{ MHz}$$

$$e_{AM} = 200 [1 + 0.8 \cos(2\pi \times 5 \times 10^3 t)] \cos(2\pi \times 1 \times 10^6 t)$$

$$e_{AM} = 200 [1 + 0.8 \cos(10^4 \pi t)] \cos(2\pi \times 10^6 t)$$

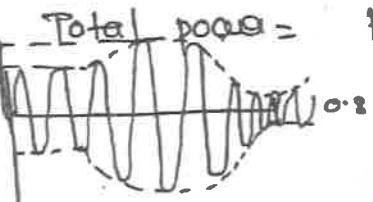
(3)  $P_{USB} = P_{LS} = \frac{m^2}{4} \times P_c = \frac{0.8^2}{4} \times 400 = 64 \text{ W.}$

$$\therefore \text{Total sideband power} = 64 \text{ W} + 64 \text{ W} = 128 \text{ W.}$$

$$\text{Total power} = P_t = P_c + P_{LSB} + P_{USB}$$

$$= 400 + 64 + 64 = 528 \text{ W.}$$

AM Wave:-



(Q3)

(3)

Q3.

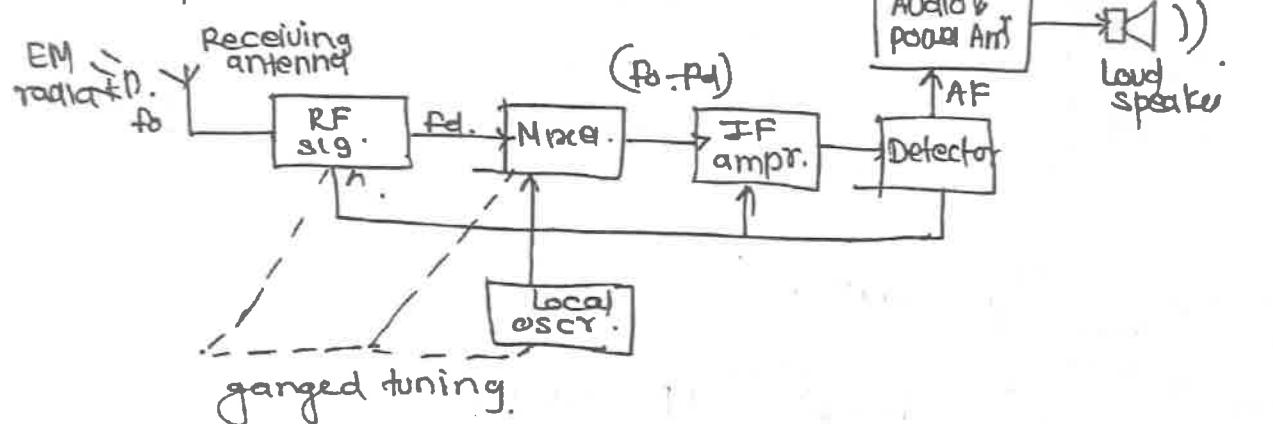
Ans b. Drawbacks of TRF.

- (1) Instability -
- (2) Variation in BLD over the tuning range
- (3) Insufficient selectivity at high frequencies and poor adjacent channel rejection.

[3N]

Explanation in short :-

- super heterodyne

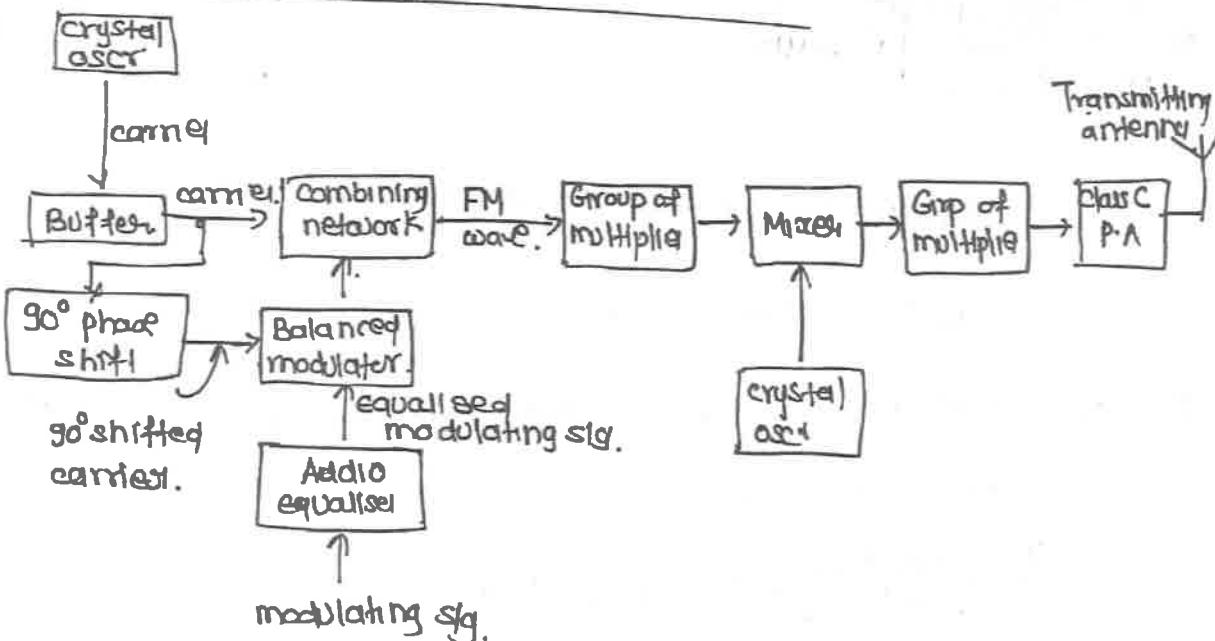


[7N]

operation in detail :

Q.4.

Ans(a) Indirect Method of FM generation:



block diagram + explanation of each block

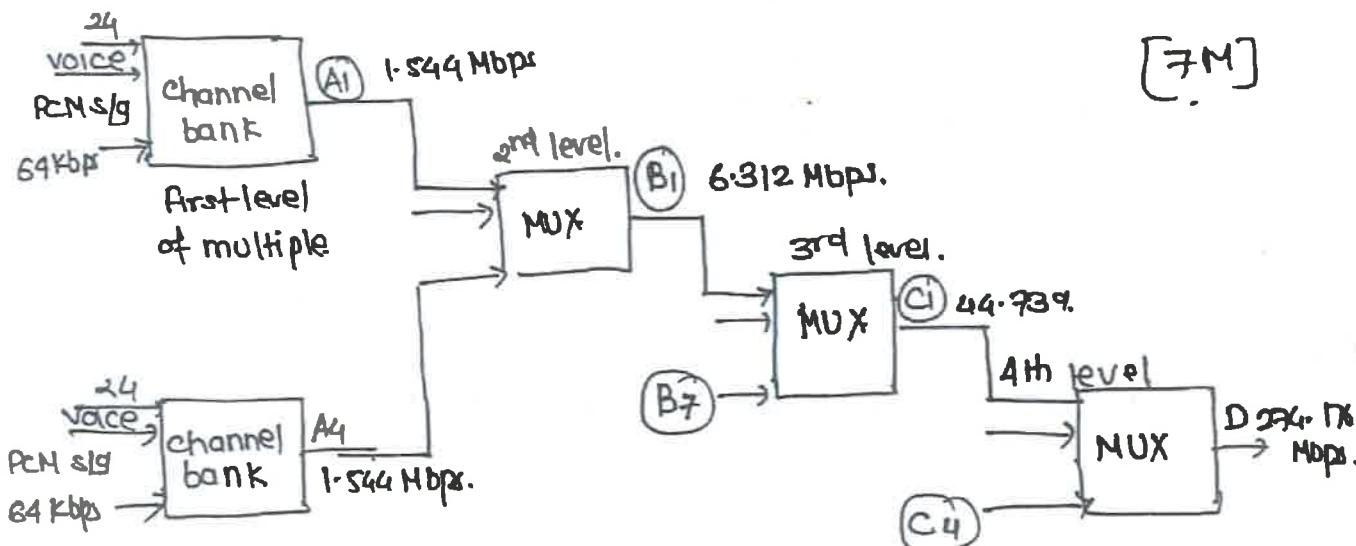
$$[3 + 7 M = 10 M]$$

06

Ans 4.b Def'n of multiplexing  
Multiplexing hierarchy

[6M]  
[2M]

Level.	AT and T.		CCIT	
	No of i/p	o/p rate Mb/s.	No of i/p	o/p rate Mb/s
First	24	1.544	30	2.048
second	4	6.312	4	8.448
third	7	44.736	4	34.368
Fourth	6	274.176	4	139.264



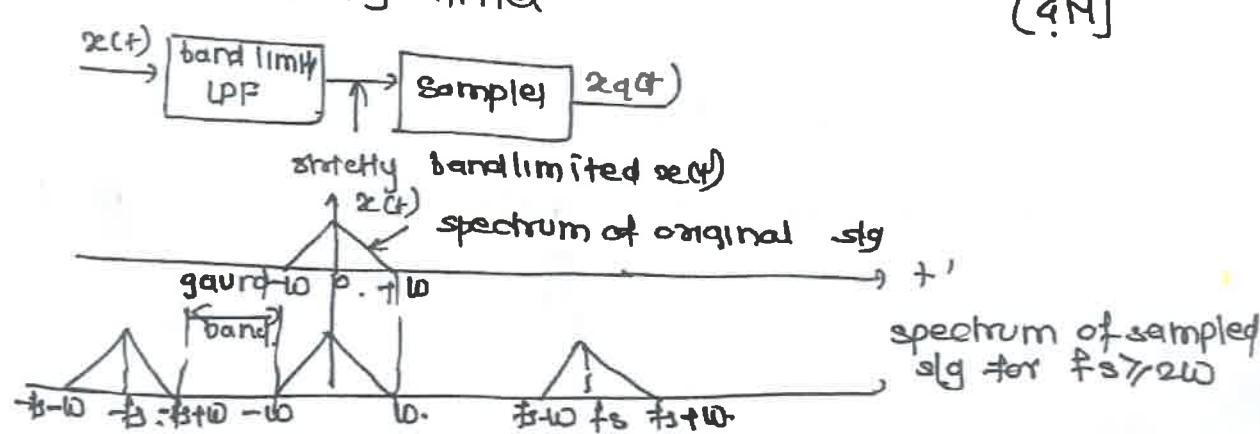
Multiplexing hierarchy for digital commn.

and explanation.

Q5. 9. Statement of sampling theorem [2M]

Anti aliasing filter

[4N]



(Q7)

(4)

(b)

$$f_1 = 20 \text{ kHz} \quad f_2 = 82 \text{ kHz}$$

[Q.7]

$$\text{BW } B = f_2 - f_1 = 82 - 20 = 62 \text{ kHz} \quad \text{--- (1)}$$

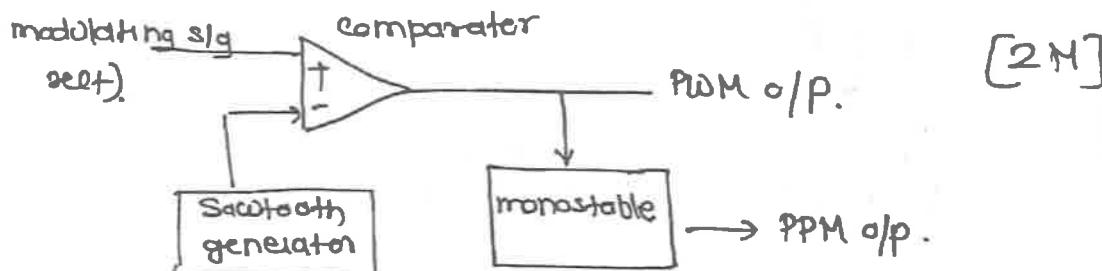
$$\text{Let us assume } f_s = 2B = 2 \times 62 = 124 \text{ kHz} \quad \text{--- (2)}$$

From eqn (1) and (2) we observe that neither  $f_1$  nor  $f_2$  is harmonically related to  $f_s$ . Hence we have to use the general bandpass sampling theorem ~~stated in preceding~~,

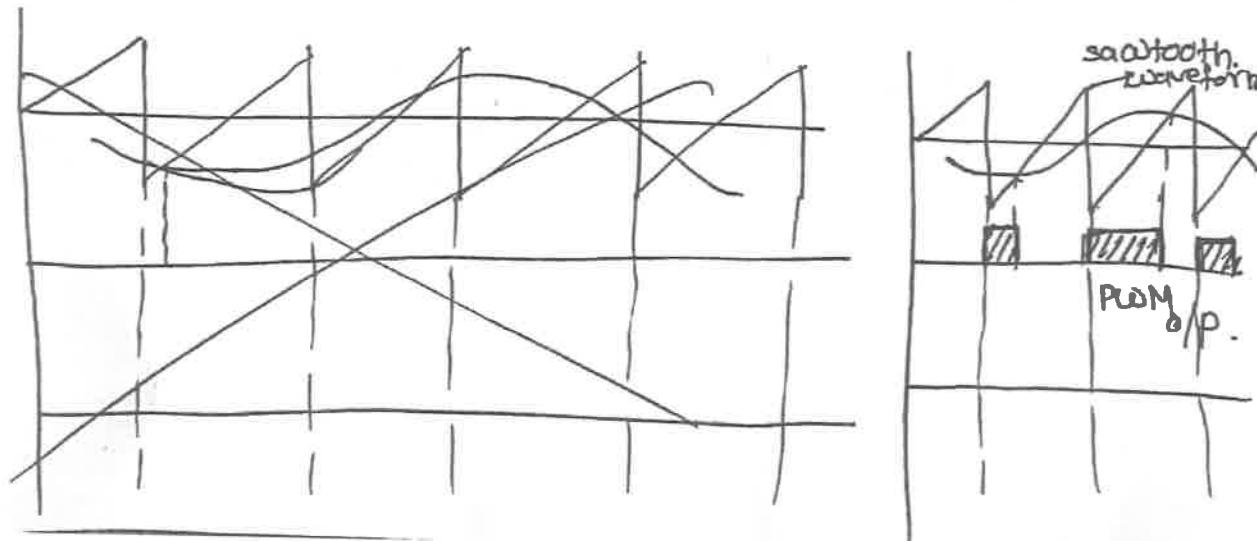
$$K = \frac{f_m}{B} = \frac{82}{62} = 1.32$$

$$f_s = \frac{2f_m}{K} = \frac{2 \times 82}{1.32} = 164 \text{ kHz}$$

Ans C. PWM generation with working



PWM generator  
Operation and explanation. →  
waveform → [5M]  
[3M]

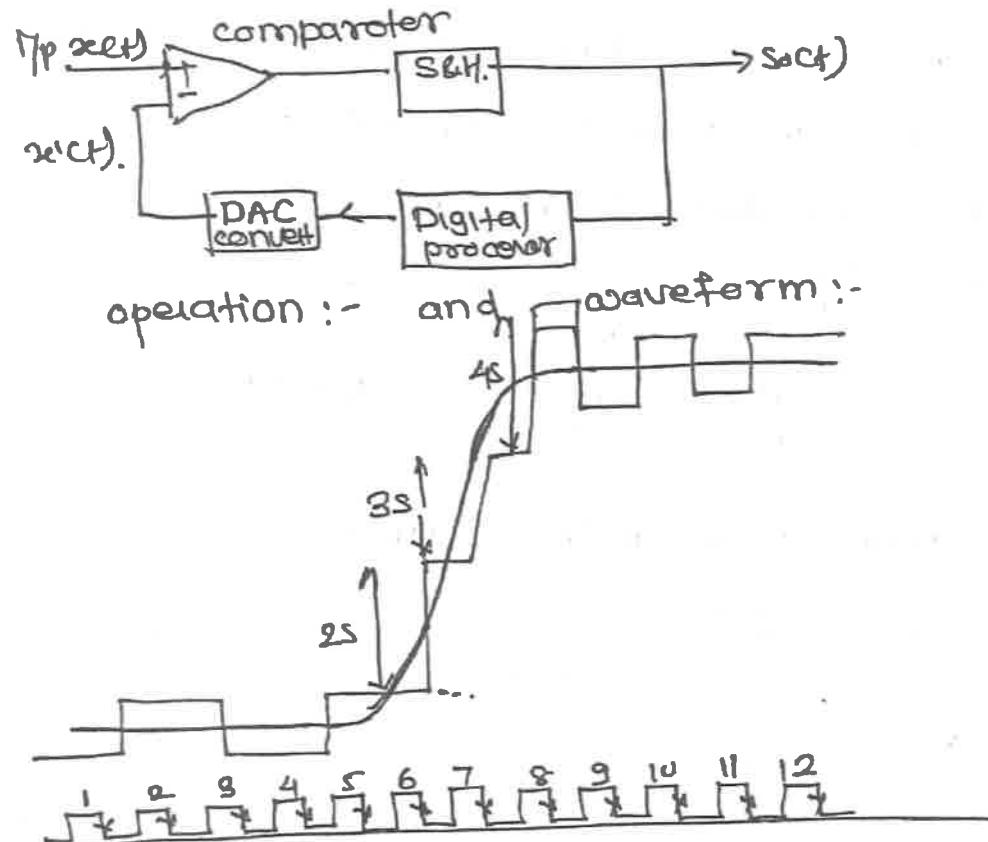


Ques 6

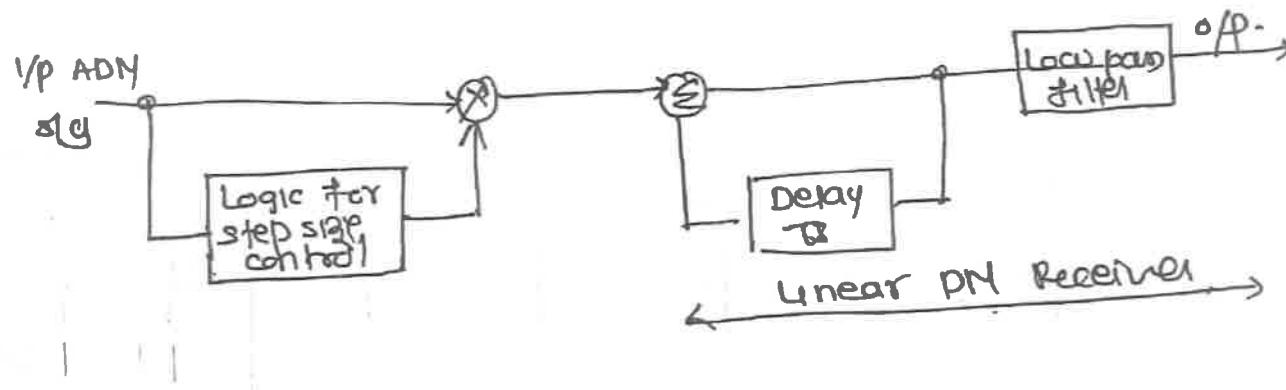
(a) Explanation for how ADM is better than  
linear delta modulation. [2M]

### ADM Transmitter

[6+2M]

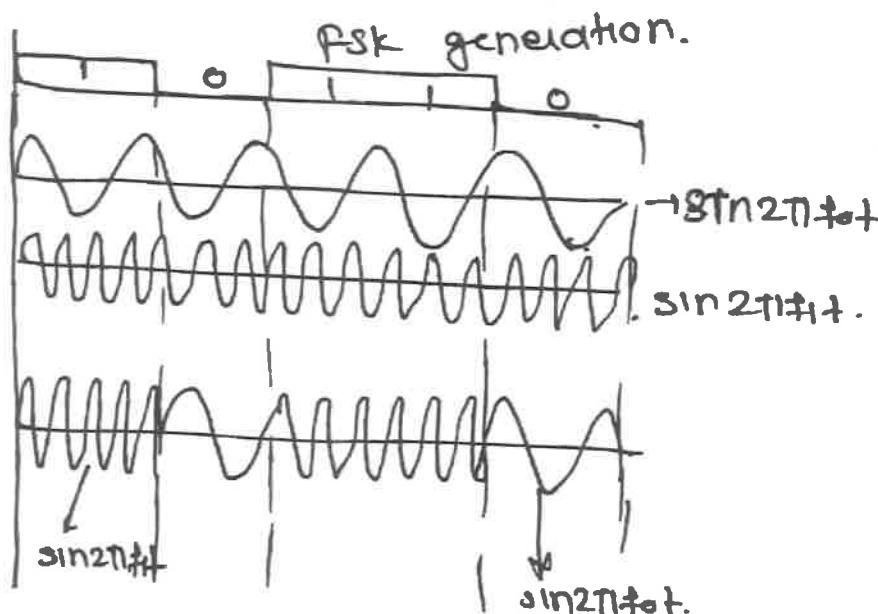
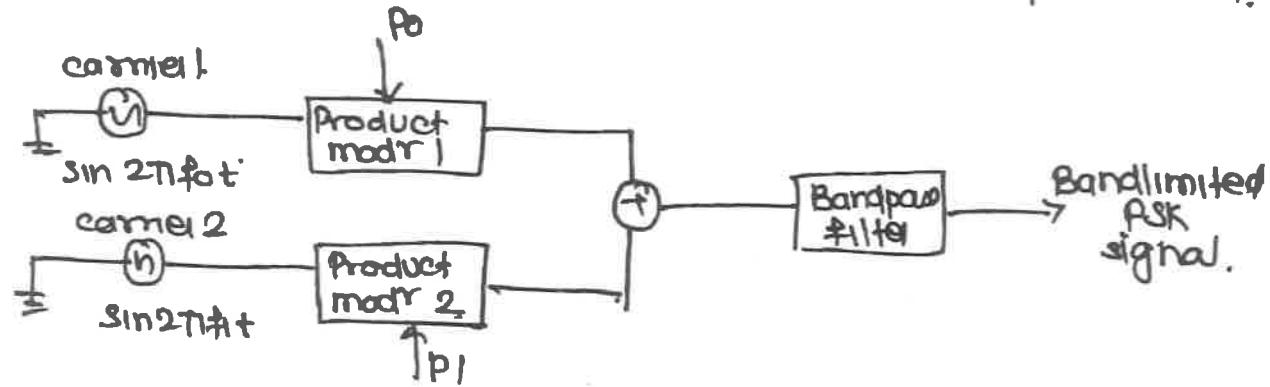


### ADM Receiver :-



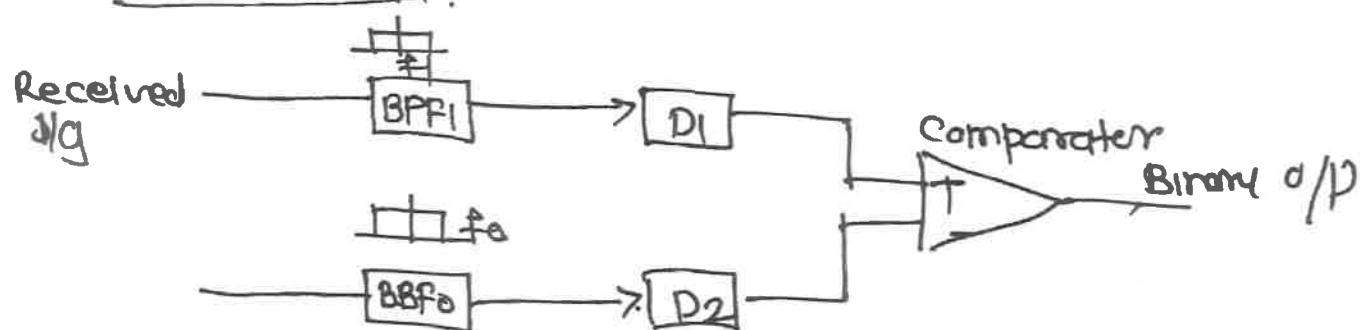
(5)

Ans 6. b. PSK generation & Modulation Reception & M.



PSK waveform.

PSK receiver.



With explanation

