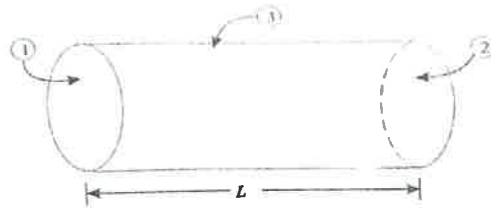


Q P code: 27944

Q10) The radiation shape factor of the circular surface of a thin hollow cylinder of 10 cm diameter and 10 cm length is 0.1716. What is the shape factor of the curved surface of the cylinder with respect to itself?

1(e)



Solution. Given: $r_1 = r_2 = \frac{10}{2} = 5 \text{ cm}; L = 10 \text{ cm}; F_{1-2} = 0.1716$

$$F_{1-2} = F_{2-1} = 0.1716 \text{ as } A_1 = A_2$$

The shape factor relation among three surfaces is given by

$$F_{1-1} + F_{1-2} + F_{1-3} = 1 \quad \dots(i)$$

$$F_{3-3} + F_{3-2} + F_{3-1} = 1 \quad \dots(ii)$$

But $F_{3-1} = F_{3-2} \quad \dots(iii)$

Also $F_{1-1} = F_{2-2} = 0$

Substituting (iii) in (ii), we get

$$F_{3-3} + F_{3-1} + F_{3-1} = 1 \quad \dots(iv)$$

$$\therefore F_{3-3} = (1 - 2F_{3-1})$$

Also $A_1 F_{1-3} = A_3 F_{3-1}$

$$\therefore F_{3-1} = F_{1-3} \times \frac{A_1}{A_3} = F_{1-3} \times \frac{\pi r^2}{2\pi r L} = F_{1-3} \times \frac{r}{2L} \quad \dots(v)$$

From eqn. (i), we have $F_{1-3} = 1 - F_{1-2}$ as $F_{1-1} = 0$
 $= 1 - 0.1716 = 0.8284 \quad \dots(vi)$

Now substituting from (vi) in (v), we get

$$F_{3-1} = 0.8284 \times \frac{5}{2 \times 10} = 0.2071 \quad \dots(vii)$$

Now substituting from (vii) in (iv), we obtain

$$F_{3-3} = 1 - 2 \times 0.2071 = 0.5858$$

Q2a) A wall of a furnace is made up of inside layer of silica brick 120 mm thick covered with a layer of magnesite brick 240 mm thick. The temperatures at the inside surface of silica brick wall and outside surface of magnesite brick wall are 725°C and 110°C respectively. The contact thermal resistance between the two walls at the interface is 0.0035°C/W per unit wall area. If thermal conductivities of silica and magnesite bricks are 1.7 W/m°C and 5.8 W/m°C, calculate.

2(a)

(i) The rate of heat loss per unit area of walls, and

(ii) The temperature drop at the interface.

Solution.

Given : $L_A = 120 \text{ mm} = 0.12 \text{ m};$
 $L_B = 240 \text{ mm} = 0.24 \text{ m};$

$$k_A = 1.7 \text{ W/m}^\circ\text{C}; k_B = 5.8 \text{ W/m}^\circ\text{C}$$

$$\text{The contact thermal resistance } (R_{th})_{cont.} = 0.0035^\circ\text{C/W}$$

The temperature at the inside surface of silica brick wall, $t_1 = 725^\circ\text{C}$

The temperature at the outside surface of the magnesite brick wall, $t_4 = 110^\circ\text{C}$

(i) The rate of heat loss per unit area of wall, q :

$$\begin{aligned} q &= \frac{\Delta t}{\sum R_{th}} = \frac{\Delta t}{R_{th-A} + (R_{th})_{cont.} + R_{th-B}} \\ &= \frac{(t_1 - t_4)}{L_A/k_A + 0.0035 + L_B/k_B} \\ &= \frac{(725 - 110)}{0.12/1.7 + 0.0035 + 0.24/5.8} \\ &= \frac{615}{0.0706 + 0.0035 + 0.0414} \end{aligned}$$

$$= 5324.67 \text{ W/m}^2$$

\therefore The rate of heat loss per unit area of wall, $q = 5324.67 \text{ W/m}^2$

(Ans.)

(ii) The temperature drop at the interface, $(t_2 - t_3)$:

As the same heat flows through each layer of composite wall, therefore,

$$q = \frac{t_1 - t_2}{L_A/k_A} = \frac{t_3 - t_4}{L_B/k_B}$$

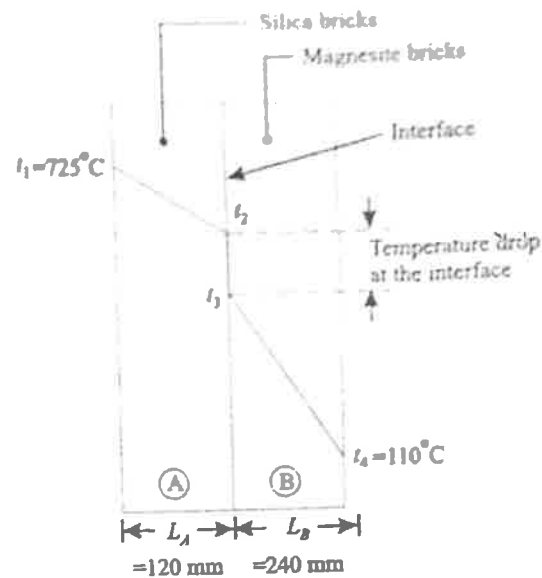
$$\text{or, } 5324.67 = \frac{(725 - t_2)}{0.12/1.7}$$

$$\text{or, } t_2 = 725 - 5324.67 \times \frac{0.12}{1.7} = 349.14^\circ\text{C}$$

$$\text{Similarly, } 5324.67 = \frac{(t_3 - 110)}{0.24/5.8}$$

$$\text{or, } t_3 = 110 + 5324.67 \times \frac{0.24}{5.8} = 330.33^\circ\text{C}$$

$$\text{Hence, the temperature drop at the interface} = t_2 - t_3 = 349.14 - 330.33 = 18.81^\circ\text{C} \quad (\text{Ans.})$$



4 (b)
 Q3 a) Air at 20°C is flowing over a flat plate which is 200 mm wide and 500 mm long. The plate is maintained at 100°C . Find the heat loss per hour from the plate if the air is flowing parallel to 500 mm side with 2 m/s velocity. What will be the effect on heat transfer if the flow is parallel to 200 mm side.

The properties of air at $(100 + 20)/2 = 60^\circ\text{C}$ are $\nu = 18.97 \times 10^{-6} \text{ m}^2/\text{s}$, $k = 0.025 \text{ W/m}\cdot\text{C}$ and $Pr = 0.7$.

Solution. Given, $U = 2 \text{ m/s}$, $\nu = 18.97 \times 10^{-6} \text{ m}^2/\text{s}$, $k = 0.025 \text{ W/m}\cdot\text{C}$ and $Pr = 0.7$.

Heat loss per hour from the plate, Q :

Case I. When the flow is parallel to 500 mm side:

$$\overline{Nu} = \frac{\bar{h} L}{k} = 0.664 (Re_L)^{1/2} (Pr)^{1/3}$$

where, $Re_L = \frac{UL}{\nu} = \frac{2 \times 0.5}{18.97 \times 10^{-6}} = 5.27 \times 10^4$

$$\begin{aligned} \bar{h} &= \frac{k}{L} \times 0.664 (Re_L)^{1/2} (Pr)^{1/3} \\ &= \frac{0.025}{0.5} \times 0.664 (5.27 \times 10^4)^{1/2} (0.7)^{1/3} = 6.767 \text{ W/m}^2\cdot\text{C} \end{aligned}$$

$$Q = \bar{h} A_s (t_s - t_\infty) = 6.767 \times (0.5 \times 0.2) (100 - 20) = 54.14 \text{ W (Ans.)}$$

Case II. When the flow is parallel to 200 mm side:

$$Re_L = \frac{2 \times 0.2}{18.97 \times 10^{-6}} = 2.11 \times 10^4$$

$$\bar{h} = \frac{0.025}{0.2} \times 0.664 \times (2.11 \times 10^4)^{1/2} (0.7)^{1/3} = 10.7 \text{ W/m}^2\cdot\text{C (Ans.)}$$

$$Q = \bar{h} \times A_s (t_s - t_\infty) = 10.7 \times (0.2 \times 0.5) \times (100 - 20) = 85.6 \text{ W (Ans.)}$$

50
 0-5) Calculate the net radiant heat exchange per m^2 area for two large parallel plates at temperatures of $427^\circ C$ and $27^\circ C$ respectively. ϵ (hot plate) = 0.9 and ϵ (cold plate) = 0.6. If a polished aluminium shield is placed between them, find the percentage reduction in the heat transfer; ϵ (shield) = 0.4.

Solution. Given: $T_1 = 427 + 273 = 700 K$; $T_2 = 27 + 273 = 300 K$; ϵ_1 (hot plate) = 0.9, ϵ_2 (cold plate) = 0.6, ϵ_3 (shield) = 0.4.

Net radiant heat exchange per m^2 area:

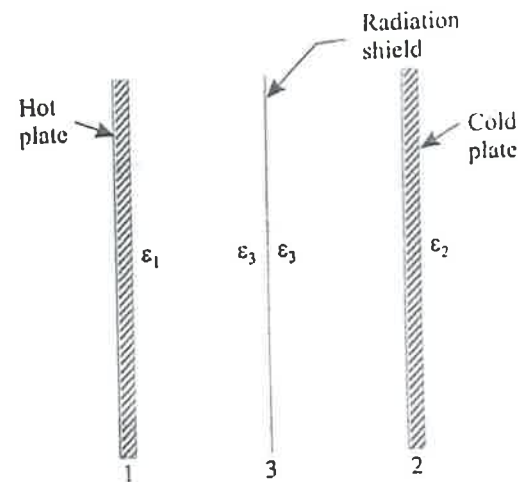
In the absence of radiation shield the heat flow between plates 1 and 2 is given by

$$\begin{aligned} (Q_{12})_{net} &= \frac{\sigma (T_1^4 - T_2^4)}{\frac{1}{\epsilon_1} + \frac{1}{\epsilon_2} - 1} \\ &= \frac{5.67 \left[\left(\frac{700}{100} \right)^4 - \left(\frac{300}{100} \right)^4 \right]}{\frac{1}{0.9} + \frac{1}{0.6} - 1} \\ &= \frac{13154.4}{1.777} = 7402.6 \text{ W. (Ans.)} \end{aligned}$$

Percentage reduction in the heat transfer flow:

When a shield is placed between the plates 1 and 2, then

$$(Q_{13})_{net} = (Q_{32})_{net}$$



$$\frac{A \sigma (T_1^4 - T_3^4)}{\frac{1}{\epsilon_1} + \frac{1}{\epsilon_3} - 1} = \frac{A \sigma (T_1^4 - T_2^4)}{\frac{1}{\epsilon_3} + \frac{1}{\epsilon_2} - 1}$$

$$\text{or, } \frac{\left(\frac{700}{100}\right)^4 - \left(\frac{T_3}{100}\right)^4}{\frac{1}{0.9} + \frac{1}{0.4} - 1} = \frac{\left(\frac{T_3}{100}\right)^4 - \left(\frac{300}{100}\right)^4}{\frac{1}{0.4} + \frac{1}{0.6} - 1}$$

$$\text{or, } \frac{2401 - x^4}{1.11 + 2.5 - 1} = \frac{x^4 - 81}{2.5 + 1.67 - 1} \quad \left[\text{where } x = \frac{T_3}{100} \right]$$

$$\text{or, } 2401 - x^4 = \frac{25.11}{25.67} (x^4 - 81) = 0.9782 (x^4 - 81)$$

$$\text{or, } 1.9782 x^4 = 2480.2 \quad \therefore x^4 = 1253.8$$

$$\text{or, } x = \frac{T_3}{100} = (1253.8)^{1/4} = 5.95 \text{ or } T_3 = 595 \text{ K}$$

$$\begin{aligned} \therefore (Q_{13})_{net} &= \frac{\sigma (T_1^4 - T_3^4)}{\frac{1}{\epsilon_1} + \frac{1}{\epsilon_3} - 1} = \frac{5.67 \left[\left(\frac{700}{100}\right)^4 - \left(\frac{595}{100}\right)^4 \right]}{\frac{1}{0.9} + \frac{1}{0.4} - 1} \\ &= \frac{6507.2}{25.11} = 259.1 \text{ W} \end{aligned}$$

\therefore Reduction in heat flow due to shield

$$= (Q_{12})_{net} - (Q_{13})_{net} = 7402.6 - 259.1 = 7143.5 \text{ W}$$

$$\text{or, } \text{Percentage reduction} = \frac{7143.5}{7402.6} \times 100 = 96.5\% \text{ (Ans.)}$$

3(b)

A counter-flow double pipe heat exchanger using superheated steam is used to heat water at the rate of 10500 kg/h. The steam enters the heat exchanger at 180°C and leaves at 130°C. The inlet and exit temperatures of water are 30°C and 80°C respectively. If overall heat transfer coefficient from steam to water is 814 W/m²°C, calculate the heat transfer area. What would be the increase in area if the fluid flows were parallel?

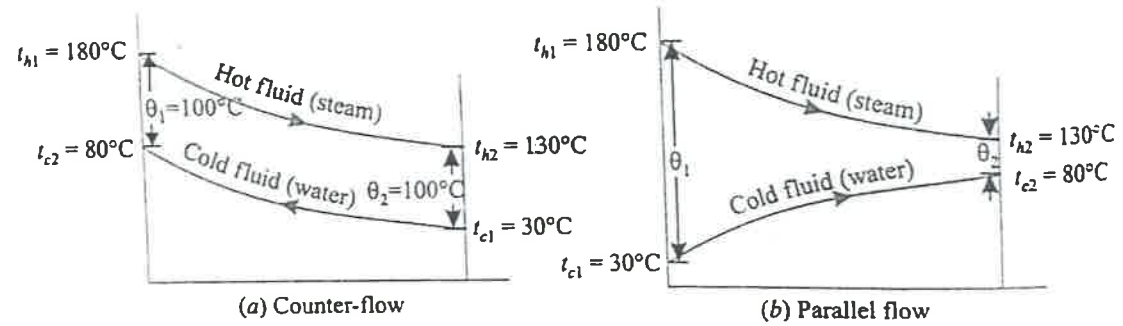
Solution. Given : $\dot{m}_w (= \dot{m}_c) = \frac{10500}{3600} = 2.917 \text{ kg/s}$; $t_{h1} = 180^\circ\text{C}$; $t_{h2} = 130^\circ\text{C}$; $t_{c1} = 30^\circ\text{C}$; $t_{c2} = 80^\circ\text{C}$; $U = 814 \text{ W/m}^2\text{°C}$.

(i) When the flow is counter :

In this

$$\theta_m = \frac{\theta_1 - \theta_2}{\ln(\theta_1/\theta_2)}$$

$$\theta_m = \theta_1 = \theta_2 = 100^\circ\text{C}$$



The heat transfer rate is given by $Q = UA \theta_m$

$$\dot{m}_c \times c_{p,c} \times (t_{c2} - t_{c1}) = UA \theta_m$$

$$2.917 \times 4.187 \times 10^3 \times (80 - 30) = 814 \times A \times 100$$

$$A = \frac{2.917 \times 4.187 \times 10^3 \times (80 - 30)}{814 \times 100} = 7.5 \text{ m}^2 \text{ (Ans.)}$$

(ii) When the flow is parallel :

$$\theta_m = \frac{\theta_1 - \theta_2}{\ln(\theta_1/\theta_2)} = \frac{(t_{h1} - t_{c1}) - (t_{h2} - t_{c2})}{\ln[(t_{h1} - t_{c1})/(t_{h2} - t_{c2})]}$$

$$= \frac{(180 - 30) - (130 - 80)}{\ln[(180 - 30)/(130 - 80)]} = \frac{150 - 50}{\ln(150/50)} = 91^\circ\text{C}$$

Again.

$$Q = UA \theta_m$$

$$\text{or } 2.917 \times (4.187 \times 10^3) \times (80 - 30) = 814 \times A \times 91$$

$$A = \frac{2.917 \times (4.187 \times 10^3) \times (80 - 30)}{814 \times 91} = 8.24 \text{ m}^2$$

$$= \frac{8.24 - 7.5}{7.5} = 0.098 \text{ or } 9.87\%$$

(Q6) An egg with mean diameter of 40 mm and initially at 20°C is placed in a boiling water pan for 4 minutes and found to be boiled to the consumer's taste. For how long should a similar egg for same consumer be boiled when taken from a refrigerator at 5°C. Take the following properties for egg:

$k = 10 \text{ W/m}^\circ\text{C}$, $\rho = 1200 \text{ kg/m}^3$, $c = 2 \text{ kJ/kg}^\circ\text{C}$ and h (heat transfer coefficient) = $100 \text{ W/m}^2\text{C}$

Use lump theory.

Solution. Given : $R = \frac{40}{2} = 20 \text{ mm} = 0.02 \text{ m}$; $t_i = 20^\circ\text{C}$; $\tau = 4 \times 60 = 240 \text{ s}$; $k = 10 \text{ W/m}^\circ\text{C}$
 $\rho = 1200 \text{ kg/m}^3$; $c = 2 \text{ kJ/kg}^\circ\text{C}$; $h = 100 \text{ W/m}^2\text{C}$.

For using the lump theory, the required condition is $B_i < 0.1$

$B_i = \frac{h L_c}{k}$ where L_c is the characteristic length which is given by,

$$L_c = \frac{V \text{ (volume)}}{A_s \text{ (surface area)}} = \frac{\frac{4}{3}\pi R^3}{4\pi R^2} = \frac{R}{3}$$

$$\therefore B_i = \frac{h}{k} \times \frac{R}{3} = \frac{100 \times 0.02}{10 \times 3} = 0.067$$

As $B_i < 0.1$, we can use lump theory.

The temperature variation with time is given by :

$$\frac{t - t_a}{t_i - t_a} = \exp \left[- \frac{h A_s}{\rho V c} \tau \right]$$

$$\frac{h A_s}{\rho V c} = \left(\frac{h}{\rho c} \right) \left(\frac{A_s}{V} \right) = \left(\frac{100}{1200 \times 2000} \right) \left(\frac{3}{R} \right)$$

$$= \left(\frac{100}{1200 \times 2000} \right) \left(\frac{3}{0.02} \right) = 0.00625$$

Substituting the values in eqn. (1), we get

$$\frac{t - 100}{20 - 100} = e^{-0.00625 \times 240} = e^{-1.50} = \frac{1}{e^{1.50}} = \frac{1}{4.4817} = 0.223$$

or, $t = 100 + (20 - 100) \times 0.223 = 82.16 \text{ }^\circ\text{C}$ say $82 \text{ }^\circ\text{C}$

Now let us find ' τ ' when the given data is : $t_i = 5^\circ\text{C}$, $t_a = 100^\circ\text{C}$ and $t = 82 \text{ }^\circ\text{C}$

Again using eqn. (1), we get

$$\frac{82 - 100}{5 - 100} = e^{-0.00625 \tau} = \frac{1}{e^{0.00625 \tau}}$$

or, $0.1895 = \frac{1}{e^{0.00625 \tau}}$ or $e^{0.00625 \tau} = 5.277$

$$0.00625 \tau = 1.6633 \text{ or } \tau = \frac{1.6633}{0.00625} = 266.13 \text{ s} = 4.435 \text{ min}$$