

Q.P Code: 25734 (TFPE sem VII)
Solution.

①

Ans 2) a) Given:- $p = 20 \text{ bar}$, $t_{\text{sup}} = 260^\circ\text{C}$,
 $m_s = 37500 \text{ kg/h}$, $t_1 = 15^\circ\text{C}$, $t_2 = 90^\circ\text{C}$,
 $m_f = 4400 \text{ kg/h}$, $C = 33000 \text{ kJ/kg}$.

1. Equivalent evaporation per kg of fuel.

$$m_e = \frac{m_s}{m_f} = \frac{37500}{4400} = \underline{\underline{8.52 \text{ kg/kg of fuel}}}$$

From steam tables, corresponding to feed water temperature of 15°C .

$$h_{f1} = 62.9 \text{ kJ/kg}.$$

Corresponding to 20 bar steam pressure,

$$h_g = 2797.2 \text{ kJ/kg}, t = 212.4^\circ\text{C}$$

Enthalpy or Total heat of 1 kg supersaturated steam

$$h_{\text{sup}} = h_g + C_p (t_{\text{sup}} - t)$$

$$= 2797.2 + 2.1 (260 - 212.4)$$

$$\boxed{h_{\text{sup}} = 2897 \text{ kJ/kg}} \quad \text{Take } C_p = 2.1 \text{ kJ/kgK}$$

Equivalent evaporation

$$E = \frac{m_e (h_{\text{sup}} - h_{f1})}{2257} = \frac{8.52 (2897 - 62.9)}{2257}$$

$$E = 10.7 \text{ kg/kg of fuel}$$

(2)

Thermal efficiency of plant

$$\eta = \frac{m_e (h_{sup} - h_{f1})}{C} = \frac{8.52(2897 - 62.9)}{33000}$$

$$\eta = 0.7317 = 73.17\%$$

∴ of Heat energy of fuel energy utilised by economiser.

From steam tables, corresponding to temp of 90°C .

$$h_{f2} = 376.9 \text{ kJ/kg}$$

Heat utilised by economiser per kg of fuel.

$$= m_e (h_{f2} - h_{f1})$$

$$= 8.52(376.9 - 62.9)$$

$$= 2675 \text{ kJ}$$

∴ of Heat utilised by economiser

$$= \frac{2675}{33000} = 0.081$$

$$= \underline{\underline{8.1\%}}$$

Q P code: 25734

(3)

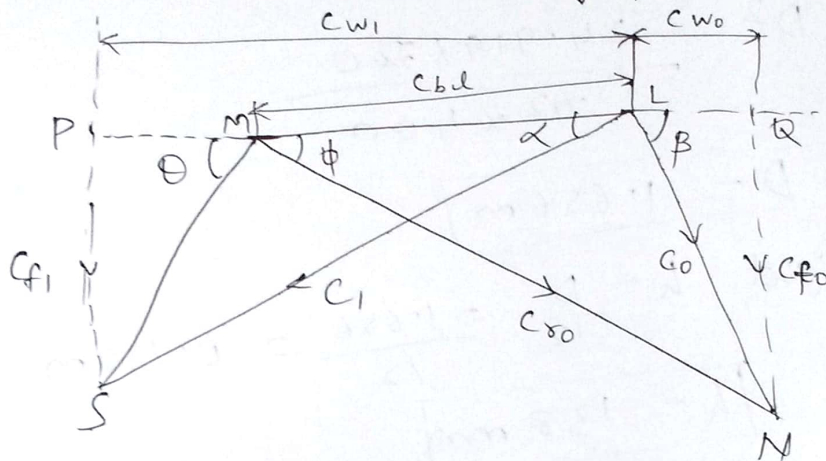
Ans 3) a)

$$N = 4000 \text{ rpm}, \alpha = 20^\circ$$

$$C_{x0} = C_1 = 1.35 C_{bl}$$

$$\dot{m}_s = 8.33 \text{ kg/s}$$

$$v = 1.381 \text{ m}^3/\text{kg}, D = 12 \text{ h}$$



Axial flow velocity,

$$\begin{aligned} C_{f1} = C_{f0} = C_f &= C_1 \sin \alpha \\ &= 1.35 C_{bl} \sin 20^\circ \\ &= 0.4617 C_{bl} \end{aligned}$$

Area of flow, $A = \pi D h$

$$A = \pi D \times \frac{D}{12} = \frac{\pi D^2}{12}$$

mass flow rate, $\dot{m} = \frac{A C_f v}{v}$

$$8.33 = \frac{(A \times 0.4617 C_{bl}) v}{1.381}$$

(4)

$$\frac{8.33 \times 1.381}{0.4917} = A \times C_{bl} = \frac{\pi D^2}{12} \times \frac{\pi D N}{60}$$

$$24.916 = \frac{\pi^2 D^3 \times 400}{720}$$

$$D^3 = \frac{24.916 \times 720}{\pi^2 \times 400}$$

$$\boxed{D = 1.656 \text{ m}}$$

$$\text{Blade height } h = \frac{D}{12} = \frac{1.656}{12} = 0.138 \text{ m}$$

$$\boxed{h = 138 \text{ mm}}$$

$$\text{Diagram work} = \dot{m} \times C_{bl} (C_{w1} + C_{w0})$$

$$= \dot{m} \times C_{bl} (2 C_1 \cos \alpha - C_{bl})$$

$$= 8.33 \times C_{bl} (2 \times 1.35 (C_{bl} \cos 20^\circ - C_{bl}))$$

$$= 8.33 \times C_{bl}^2 \cdot (2 \times 1.35 \cos 20^\circ - 1)$$

$$= 8.33 \times \left(\frac{\pi D N}{60} \right)^2 \times 1.537$$

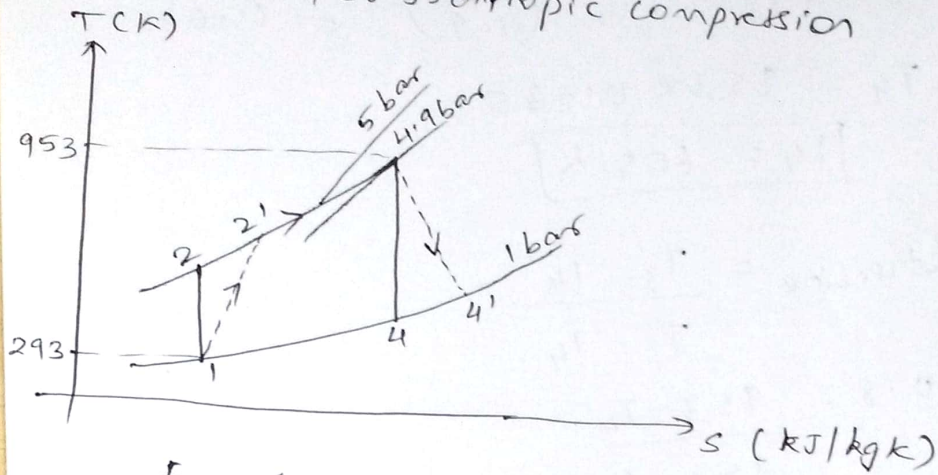
$$= 15401.2 \text{ W}$$

$$\text{Diagram work} = \underline{\underline{15.4 \text{ kW}}}$$

Q P Code:- 25734

(5)

Ans 6) a) Quantity of air circulation:-
For Isentropic compression



for Isentropic compression 1-2,

$$\frac{T_2}{T_1} = \left(\frac{P_2}{P_1}\right)^{\gamma-1/\gamma}$$

$$\frac{T_2}{T_1} = \left(\frac{5}{1}\right)^{\frac{1.4-1}{1.4}} = 1.584$$

$$T_2 = 293 \times 1.584 = 464 \text{ K}$$

$$\boxed{T_2 = 464 \text{ K}}$$

$$\eta_{\text{Compressor}} = \frac{T_2 - T_1}{T_2' - T_1} \Rightarrow$$

$$0.85 = \frac{464 - 293}{T_2' - 293}$$

$$T_2' = \frac{464 - 293}{0.85} + 293$$

$$\therefore \boxed{T_2' = 494 \text{ K}}$$

For isentropic expansion process 3-4,

(6)

$$\frac{T_4}{T_3} = \left(\frac{P_4}{P_3}\right)^{\frac{\gamma-1}{\gamma}} = \left(\frac{1}{4.9}\right)^{\frac{1.4-1}{1.4}} = 0.635$$

$$T_4 = 953 \times 0.635$$

$$\boxed{T_4 = 605 \text{ K}}$$

$$\eta_{\text{turbine}} = \frac{T_3 - T_4'}{T_3 - T_4}$$

$$0.8 = \frac{953 - T_4'}{953 - 605}$$

$$T_4' = 953 - 0.8(953 - 605)$$

$$T_4' = 674.6 \text{ K}$$

$$\begin{aligned} W_{\text{compressor}} &= c_p(T_2' - T_1) \\ &= 1.024(494 - 293) \\ &= 205.8 \text{ kJ/kg} \end{aligned}$$

$$\begin{aligned} W_{\text{turbine}} &= c_p(T_3 - T_4') \\ &= 1.024(953 - 674.6) \\ &= 285.1 \text{ kJ/kg} \end{aligned}$$

$$\begin{aligned} W_{\text{net}} &= W_{\text{turbine}} - W_{\text{compressor}} \\ &= 285.1 - 205.8 \end{aligned}$$

$$\boxed{W_{\text{net}} = 79.3 \text{ kJ/kg of air}}$$

6) a) (Continue)

(7)

If mass of air flowing is m_a kg/sec

$$P = m_a \times w_{het} \text{ kW}$$

$$1065 = m_a \times 79.3$$

$$\boxed{m_a = 13.43 \text{ kg}}$$

Quantity of air circulation = 13.43 kg

Heat supplied per kg of air circulation:-

Actual heat supplied per kg of air circulation:-

$$= \frac{c_p (T_3 - T_2')}{\eta_{\text{combustion}}} = \frac{1.024 (953 - 494)}{0.85}$$

$$= \underline{\underline{552.9 \text{ kJ/kg}}}$$

Thermal efficiency of cycle η_{thermal} :

$$\eta_{\text{thermal}} = \frac{\text{Work output}}{\text{Heat supplied}}$$

$$= \frac{79.3}{552.9}$$

$$= 0.1434$$

$$\boxed{\eta_{\text{thermal}} = 14.34 \%}$$